



~~Attorney Docket No. 2856-04US01~~

**A**  
**GAS INFLATION/EVACUATION SYSTEM AND SEALING SYSTEM  
FOR GUIDEWIRE HAVING OCCLUSIVE DEVICE**

**ASSEMBLY**

RELATED APPLICATIONS

- 5 The present invention is related to two co-pending applications that are commonly assigned to the assignee of the present invention and filed concurrently herewith, the first of which is entitled "GUIDEWIRE OCCLUSION SYSTEM UTILIZING REPEATABLY INFLATABLE GAS-FILLED OCCLUSIVE DEVICE," ~~[Serial]~~ <sup>Application 10/012,903</sup> No. ~~09/xxx,xxx (Attorney Docket No. 2856-02US01)~~, and the second of which is entitled "GUIDEWIRE HAVING
- 10 OCCLUSIVE DEVICE AND REPEATABLY CRIMPABLE PROXIMAL END," <sup>Application 10/012,891</sup> ~~[Serial]~~ No. ~~09/xxx,xxx (Attorney Docket No. 2856-03US01)~~, a copy of each of which is attached and the disclosure <sup>of</sup> of both, which are incorporated by reference.

FIELD OF THE INVENTION

- 15 The present invention relates generally to the field of vascular medical devices. More specifically, the present invention relates to a gas inflation/evacuation system <sup>and sealing system</sup> for selectively and repeatedly inflating an <sup>occlusive</sup> ~~occlusion~~ balloon and crimping <sup>an extended sealable section proximal</sup> the proximal end of a guidewire <sup>assembly</sup> during an occlusion procedure.

20 BACKGROUND OF THE INVENTION

- Arterial disease involves damage that happens to the arteries in the body. Diseased <sup>arteries</sup> ~~vessels~~ can become plugged with thrombus, plaque, or grumous material that may ultimately lead to a condition known as ischemia. Ischemia refers to a substantial reduction or loss of blood flow to the heart muscle or any other tissue that is being supplied by the artery and can lead to
- 25 permanent damage of the affected region. While arterial disease is most commonly associated with the formation of hard plaque and coronary artery disease in the heart, similar damage can happen to many other vessels in the body, such as the peripheral vessels, cerebral vessels, due to the build up of hard plaque or softer thrombus or grumous material within the lumen of an artery or vein.

A variety of vascular medical devices and procedures have been developed to treat diseased vessels. The current standard procedures include bypass surgery (where a new blood vessel is grafted around <sup>a</sup>the narrowed or blocked artery) and several different types of non-surgical interventional vascular medical procedures, including angioplasty (where a balloon on a catheter is inflated inside <sup>a</sup>the narrowed or blocked portion of <sup>a</sup>the artery in an attempt to push back <sup>a</sup>the plaque or thrombotic material), stenting (where a metal mesh tube is expanded against <sup>a</sup>the narrowed or blocked portion of <sup>a</sup>the artery to hold back <sup>a</sup>the plaque or thrombotic material), and debulking techniques in the form of atherectomy (where some type of high speed or high power mechanism is used to dislodge <sup>a</sup>the hardened plaque) or thrombectomy (where some type of mechanism or infused fluid is used to dislodge grumous <sup>or</sup>thrombotic material). In each of these <sup>interventional</sup> vascular medical procedures, a very flexible guidewire is routed through the patient's vascular system to a desired treatment location and then a catheter that includes a device on the distal end appropriate for the given procedure is tracked along the guidewire to the treatment location.

Although interventional vascular procedures avoid many of the complications involved in surgery, there is a possibility of complications if some of the plaque, thrombus or other material breaks free and flows downstream in the artery <sup>or other vessel</sup>, potentially causing a stroke, a myocardial infarction (heart attack), or other tissue death. One solution to this potential complication is to use some kind of occlusive device to block or screen the blood flowing downstream of the treatment location. Examples of catheter arrangements that use a pair of balloons as occlusive devices to create an isolated space in the blood vessel are described in U.S. Patent Nos. 4,573,966, 4,636,195, 5,059,178, 5,320,604, 5,833,644, 5,925,016, 6,022,336 and 6,176,844. Examples of catheter arrangements that use a single balloon as an occlusive device either upstream or downstream of the treatment location are described in U.S. Patent Nos. 5,171,221, 5,195,955, 5,135,482, 5,380,284, 5,688,234, 5,713,917, 5,775,327, 5,792,179, 5,807,330, 5,833,650, 5,843,022, 6,021,340, 6,159,195 and 6,248,121. An example of a catheter arrangement that uses a mechanically-expanded <sup>occlusive</sup> ~~occlusion~~ device is shown in U.S. Patent No. 6,231,588. Occlusive balloons also have been used on non-over-the-wire catheters without any guidewire internal to the catheter as described, for example, in U.S. Patent Nos. 4,838,268 and 5,209,727.

The use of an occlusive device as part of a vascular procedure is becoming more common in debulking procedures performed on heart bypass vessels. Most heart bypass vessels are harvested and transplanted from the saphenous vein located along the inside of the patient's leg. The saphenous vein is a long, straight vein that has a capacity more than adequate to support the blood flow needs of the heart. Once transplanted, the saphenous vein is subject to <sup>a buildup of</sup> arterial ~~disease caused by~~ plaque or thrombotic materials ~~that built up~~ in the grafted arterial lumen. Unfortunately, the standard interventional vascular treatments for debulking are only moderately successful when employed to treat saphenous vein coronary bypass grafts. The complication rate for a standard balloon angioplasty procedure in a saphenous vein coronary bypass graft is higher than in a native vessel with the complications including embolization, "no-reflow" phenomena, and procedural related myocardial infarction. Ather<sup>o</sup>ectomy methods including directional, rotational, and laser devices are also associated with a high degree of embolization resulting in a greater likelihood of infarction. The use of stents for saphenous vein coronary bypass grafts has produced mixed results. Stents provide for less restenosis, but they do not eliminate the risk of embolization and infarction <sup>incurred by standard balloon angioplasty</sup>.

In order to overcome the shortcomings of these standard non-surgical interventional treatments in treating saphenous vein coronary bypass graft occlusion, embolic protection methods utilizing a protective device distal to the lesion have been developed. The protective device is typically a filter or a balloon. Use of a protective device in conjunction with an ather<sup>o</sup>ectomy or thrombectomy device is intended to prevent emboli from migrating beyond the protective device and <sup>to</sup> allow the embolic particles to be removed, thereby subsequently reducing the risk of myocardial infarction. When the occlusive device is a balloon, the balloon is inserted and inflated at a point distal to the treatment site or lesion site. Therapy is then performed at the treatment site and the balloon acts to block all blood flow which prevents emboli from traveling beyond the balloon. Following treatment, some form of particle removal device must be used to remove the dislodged emboli prior to balloon deflation. U.S. Patent <sup>No.</sup> 5,843,022 uses a balloon to occlude the vessel distal to a lesion or blockage site. The occlusion is treated with a high pressure water jet and the fluid and entrained emboli are subsequently removed via an extraction

No.  
tube. U.S. Patent 6,135,991 describes the use of a balloon to occlude the vessel allowing blood flow and pressure to prevent the migration of emboli proximally from the treatment device.

There are various designs that have included an occlusive balloon on the end of a guidewire. U.S. Patent Nos. 5,520,645, 5,779,688 and 5,908,405 describe guidewires having removable ~~occlusion~~<sup>occlusive</sup> balloons on a distal end. U.S. Patent No. 4,573,470 describes a guidewire having an ~~occlusion~~<sup>occlusive</sup> balloon where the guidewire is bonded inside the catheter as an integral unit. U.S. Patent Nos. 5,059,176, 5,167,239, 5,520,645, 5,779,688 and 6,050,972 describe various guidewires with balloons at the distal end in which a valve arrangement is used to inflate and/or deflate the balloon. U.S. Patent No. 5,908,405 describes an arrangement with a removable  
10 balloon member that can be repeatedly inserted into and withdrawn from a guidewire. U.S. Patent No. 5,776,100 describes a guidewire with an occlusive balloon adhesively bonded to the distal end with an adapter on the proximal end to provide inflation fluid for the occlusive balloon.

<sup>normal</sup>  
Except in the case of the cerebral anatomy where there are redundant arteries supplying  
15 blood to the same tissue, one of the problems with using an occlusive device in the arteries is that tissue downstream of the occlusive device can be damaged due to the lack of blood flow. Consequently, an occlusive device that completely blocks the artery can only be deployed for a relatively short period of time. To overcome this disadvantage, most of the recent development in relation to occlusive devices has focused on devices that screen the blood through a filter  
20 arrangement. U.S. Patent Nos. 5,827,324, 5,938,672, 5,997,558, 6,080,170, 6,171,328, 6,203,561 and 6,245,089 describe various examples of filter arrangements that are to be deployed on the distal end of a catheter system. While a filter arrangement is theoretically a better solution than an occlusive device, in practice such filter arrangements often become plugged, effectively turning the filter into an occlusive device. The filter arrangements also are  
25 mechanically and operationally more complicated than an occlusive balloon device in terms of deployment and extraction.

As is the case in almost all angioplasty devices or stenting catheter devices where a balloon is used to expand the blood vessel or stent, most catheter ~~balloon~~<sup>balloons</sup> occlusive ~~devices~~<sup>balloons</sup> as well as most guidewire ~~balloon~~<sup>balloons</sup> occlusive ~~devices~~<sup>balloons</sup> utilize a liquid fluid such as saline or saline

mixed with a radiopaque marker for fluoroscopic visualization (i.e., contrast) as the inflation medium ~~[for the balloon]~~. Generally, a liquid fluid medium for expanding vascular balloons has been preferred because the expansion characteristics of a liquid are more uniform and predictable, and because a liquid medium is easier to work with and more familiar to the doctors.

5 In the case of angioplasty balloons, for example, high-pressure requirements (up to 20 atmospheres) necessitate that the inflation fluid be an incompressible fluid for safety reasons. While having numerous advantages, liquid fluids do not lend themselves to rapid deflation of an occlusive balloon because of the high resistance to movement of the liquid in a long small diameter tube. In the context of angioplasty procedures, the balloon catheter has a much larger  
10 lumen than a guidewire. Consequently, rapid deflation is possible. In the context of a guidewire, however, liquid filled ~~[occlusion]~~<sup>occlusive</sup> balloons typically cannot be deflated in less than a minute and, depending upon the length of the guidewire, can take up to several minutes to deflate. Consequently, it is not practical to shorten the period of total blockage of a vessel by repeatedly deflating and then re-inflating a liquid filled occlusive balloon at the end of a guidewire.

15 Gas-filled balloons have been used for intra-aortic ~~[occlusion]~~<sup>occlusive</sup> devices where rapid inflation and deflation of the ~~[occlusion]~~<sup>occlusive</sup> device is required. Examples of such intra-aortic ~~[occlusion]~~<sup>occlusive</sup> devices are shown in U.S. Patent Nos. 4,646,719, 4,733,652, 5,865,721, 6,146,372, 6,245,008 and 6,241,706. While effective for use as an intra-aortic ~~[occlusion]~~<sup>occlusive</sup> device, these  
20 ~~[occlusion]~~<sup>occlusive</sup> devices are not designed for use as a guidewire as there is no ability to track a catheter over the intra-aortic ~~[occlusion]~~<sup>occlusive</sup> device.

An early catheter balloon device that utilized a gas as an inflation medium and provided a volume limited syringe injection system is described in U.S. Patent No. 4,865,587. More recently, a gas-filled ~~[occlusion]~~<sup>occlusive</sup> balloon on a guidewire is described as one of the alternate embodiments in U.S. Patent No. 6,217,567. The only suggestion for how the guidewire of the  
25 alternate embodiment is sealed is a valve type arrangement similar to the valve arrangement used in a liquid fluid embodiment. A similar gas-filled ~~[occlusion]~~<sup>occlusive</sup> balloon has been described with respect to the Aegis Vortex™ system developed by Kensey Nash Corporation. In both U.S. Patent No. 6,217,567 and the Aegis Vortex™ system, the gas-filled occlusive balloon is used for distal protection to minimize the risk of embolization while treating a blocked saphenous vein

coronary bypass graft. Once deployed, the occlusive balloon retains emboli dislodged by the atherectomy treatment process until such time as the emboli can be aspirated from the vessel. No specific apparatus are shown or described for how the gas is to be introduced into the device or how the <sup>occlusive</sup> balloon is deflated.

5 Although the use of occlusive devices has become more common for distal embolization protection in vascular procedures, particularly for treating a blocked saphenous vein coronary bypass graft, all of the existing approaches have significant drawbacks that can limit their effectiveness. Liquid filled occlusive balloons can remain in place too long and take too long to deflate, increasing the risk of damages downstream of the occlusion. Occlusive filters are  
10 designed to address this problem, but suffer from blockage problems and can be complicated to deploy and retrieve and may allow small embolic particles to migrate downstream. Existing gas-filled occlusive balloons solve some of the problems of liquid filled occlusive balloons, but typically have utilized complicated valve and connection arrangements. It would be desirable to provide for an occlusive device that was effective, simple, quick to deploy and deflate, and that  
15 could overcome the limitations of the existing approaches.

→ that has a distal portion and a proximal portion with an extended sealable section

### SUMMARY OF THE INVENTION

The present invention is a gas inflation/evacuation system <sup>and sealing system</sup> for use with occlusive devices in vascular procedures. The gas inflation/evacuation system is removably <sup>connectible</sup> connectable to <sup>the</sup> a

20 proximal end of a <sup>tubular</sup> guidewire assembly and includes an evacuation <sup>syringe</sup> system to evacuate <sup>the</sup> air from the guidewire and an inflation <sup>syringe or syringes</sup> system for introducing a gas under pressure into the guidewire to inflate an occlusive balloon <sup>or other occlusive device proximate the distal end of the tubular guidewire assembly</sup> a plurality of times. A sealing system is also removably <sup>connectible</sup> connectable to the proximal end of the <sup>tubular</sup> guidewire assembly and selectively seals the <sup>tubular guidewire assembly</sup> proximal end at one of a plurality of separate locations <sup>along the extended sealable section tubular assembly</sup> to form an airtight seal of the guidewire. Each time a deflation of <sup>balloon in order</sup> the occlusive <sup>balloon</sup> device is desired to reestablish blood flow to the vessel downstream of the occlusive <sup>extended sealable section</sup> device, the proximal end of the <sup>balloon</sup> guidewire preferably is cut distal to the location of the last seal to quickly deflate the occlusive <sup>gas inflation/evacuation and sealing system</sup> device.

The advantage of the <sup>gas inflation/evacuation and sealing system</sup> guidewire occlusion system of the present invention is that the occlusive device can be repeatably inflated and deflated a plurality of times during a vascular

procedure in between which the proximal end of the guidewire is free of mechanical connections and obstructions and functions as a conventional exchange guidewire for one or more over-the-wire catheters. Alternatively, the guidewire assembly of the present invention can be shorter in length for use with rapid exchange catheter systems. Unlike existing liquid filled occlusive devices, the present invention is capable of repeated and quick inflation and deflation which allows an operator to deploy the gas-filled occlusive device numerous times during a procedure for shorter periods of time, thereby reducing the risk of potential damage to downstream tissue. Unlike other gas-filled occlusive devices, the present invention is simple and permits the guidewire to be used as a conventional exchange guidewire. There are no complicated mechanical arrangements or valve systems internal to the guidewire that increase the cost, complexity and potential for failure of the system.

In a preferred embodiment, the extended sealing section is a crimpable section and the sealing mechanism is a crimping mechanism. The crimpable section has a sufficient length to permit a plurality of crimps and cuts along the crimpable section and preferably has an outer diameter that is smaller than or equal to a diameter of the main body of the guidewire. The crimping mechanism is used to crimp the crimpable section of the guidewire to seal the guidewire a plurality of times. Preferably, the gas inflation/evacuation system and the crimping mechanism of the sealing system are arranged as parts of a handheld apparatus. Each time a deflation of the occlusive device is desired to reestablish blood flow to the vessel downstream of the occlusive device, the crimpable section is cut distal to the location of the last crimp so as to quickly deflate the occlusive device. Preferably, the extended crimpable section of the guidewire is dimensioned and the crimping mechanism is arranged such that an effective outer diameter of the crimpable section at the location of a seal is no greater than the outer diameter of the main body of the guidewire assembly when the crimpable section is sealed.

In an alternate embodiment, the sealing mechanism is a plugging mechanism that selectively inserts a plug of material into the distal end of the sealable section while maintaining an airtight seal between the guidewire assembly and the inflation/evacuation system. In one embodiment, the plug of material includes a wax/gel material and the sealing system includes wiping structure to remove excess wax/gel material from the outside of the sealable section

once the wax/gel material has been inserted. In this embodiment, the <sup>extended</sup>sealable section may be opened either by cutting the <sup>extended</sup>sealable section distal to the location of the seal or by heating the <sup>extended</sup>proximal end of the sealable section.

In one embodiment for coronary vascular procedures, the guidewire assembly preferably  
5 has an effective length of at least 40 cm and more preferably at least 100 cm and an outer diameter of less than 0.060 inches and more preferably less than 0.018 inches, the extended sealable section has an effective length of at least 1 cm and more preferably at least 5 cm and an outer diameter of less than 0.050 inches and more preferably less than 0.012 inches, and the occlusive device <sup>(balloon)</sup>is deflated in less than two minutes and more preferably less than one minute.  
10 This embodiment is particularly adapted to provide distal embolization protection in debulking vascular interventional procedures, such as those involving a blocked saphenous vein coronary bypass graft. Alternatively, the ~~guidewire occlusion system and~~ guidewire assembly may be configured and dimensioned for use in peripheral vascular procedures or <sup>neurovascular</sup>~~neural vascular~~ procedures.

15 In a preferred embodiment, the inflation system of the gas <sup>inflation/evacuation</sup>~~inflation~~ system includes a plurality of individually <sup>actuatable</sup>~~actuable~~ syringes each containing a sufficient volume of biocompatible gas for a single inflation of the occlusive device so as to minimize the volume of biocompatible gas in the <sup>gas inflation/evacuation</sup>system in the event of a leak. The preferred embodiment is packaged in a sterile packaging that is assembled and packaged in a <sup>sealed chamber</sup>~~vessel~~ filled with a biocompatible gas such that  
20 any gas within the sterile packaging once packaged is only the biocompatible gas.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic diagram of a guidewire occlusion system <sup>incorporating</sup>~~in accordance with~~ the present invention <sup>and</sup> operating in an evacuation mode.

25 Fig. 2 is a schematic diagram of the <sup>guidewire occlusion system</sup>~~embodiment~~ shown in Fig. 1 operating in an inflation mode.

Fig. 3a <sup>is a</sup> and Fig. 3b are side views of the guidewire assembly shown in Fig. 1. <sup>and Fig. 3b is an enlarged view of the portion of Fig. 3a delineated by the circle 3b</sup>

Figs. 4a and 4b are <sup>fragmentary</sup>cross-sectional views of the proximal portion of the guidewire assembly of Fig. 3a. <sup>different manners of joining the extended sealable section to the main body portion at</sup>



three  
Figs. 5-7 are perspective views of alternate embodiments of ~~the inflation/deflation~~  
system ~~gas inflation/evacuation systems and the sealing systems used therewith~~

Fig. 8 is an exploded view of the gas inflation/evacuation system of the alternate  
embodiment shown in Fig. 7 ~~and the associated sealing system~~

5 Fig. 9 is a perspective view of the ~~crimping mechanism of~~ ~~the alternate embodiment~~  
shown in Fig. 7. ~~a gas inflation/evacuation system and sealing~~

Fig. 10 is a top view of a preferred embodiment of ~~the inflation/deflation~~ system of the  
present invention.

10 Fig. 11 is a perspective view of ~~an alternate embodiment of the~~ ~~gas inflation/evacuation~~  
system ~~and sealing system~~

Fig. 12 is an end view of ~~the handheld apparatus for the sealing system in accordance~~  
~~with one embodiment of the present invention.~~ ~~a crimping mechanism~~

Figs. 13 and 14 are two sectional views of ~~the sealing system~~ of Fig. 12 ~~crimping mechanism~~

15 Fig. 15 is a cross-sectional view of an alternate embodiment of ~~the~~ ~~sealing system~~  
showing one embodiment of a plugging mechanism.

Fig. 16 is a ~~perspective~~ ~~view of the preferred~~ ~~sealed chamber for packaging and~~  
~~assembling in accordance with the present invention.~~ ~~the guidewire occlusion system~~ ~~use in assembling and~~

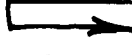
Fig. 17 is a side view of a biocompatible packaging ~~in accordance with one embodiment~~  
~~of the present invention.~~

20 Fig. 18 is an exploded view of ~~an alternate embodiment of the~~ ~~gas inflation/evacuation~~  
system ~~and sealing system~~

Fig. 19 is a ~~perspective~~ ~~view of a joinable housing assembly for an alternate embodiment~~  
~~of the gas inflation/evacuation system.~~ ~~partially exploded the alternate embodiment of Fig. 18 including the entire~~ ~~thereof~~

## 25 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring now to Figs. 1-2, the overall operation of a guidewire occlusion system 20 ~~in~~  
~~accordance with~~ ~~the present invention~~ will be described. The guidewire occlusion system 20  
includes a guidewire assembly 22, a sealing system 60, and a gas inflation/evacuation system 80.  
The preferred embodiments of the overall guidewire occlusion system 20 are described in further

9  Fig. 14 being a view taken along the  
line 14-14 of Fig. 12, and Fig. 13 being  
a magnification of the portion of Fig. 14  
indicated by the dashed circle

10/012,903

detail in the previously identified co-pending application entitled "Guidewire Occlusion System Utilizing Repeatably Inflatable Gas-Filled Occlusive Device".

Guidewire assembly 22 is a tubular member that includes a proximal portion 24 and a distal portion 26. As used in the present invention, the terms proximal and distal will be used with reference to an operator ~~of the device~~ such that a distal portion of the ~~device of the~~ guidewire assembly 22, for example, is the portion first inserted into a blood vessel, and the proximal portion remains exterior to the patient and is therefore closer to the operator ~~of the device~~. An extended sealable section 28 is provided proximate the proximal portion 24 of guidewire assembly 22. Preferably, the <sup>extended</sup> sealable section 28 is <sup>an extended</sup> a crimpable section comprised of a tubular segment having an outer diameter smaller than an outer diameter of a main body portion 30 of guidewire assembly 22. Although the diameter of the <sup>extended</sup> crimpable section could be any size consistent with effective use as a guidewire, it will be understood that the smaller diameter allows for less force to be used in sealing the <sup>extended</sup> crimpable section and provides a crimped seal that is not too large when crimped. An occlusive balloon 32 is located along the distal portion 26 of guidewire assembly 22. The occlusive balloon 32 is fluidly connected via a lumen 34 to <sup>the</sup> ~~the~~ proximal end 36 ~~of proximal portion 24~~ of guidewire assembly 22, with channels or holes 35 allowing for fluid communication between lumen 34 and <sup>occlusive</sup> balloon 32. In a preferred embodiment, a flexible tip 38 is positioned at the distal end 40 of distal portion 26 of the guidewire assembly 22. Preferably, distal portion 26 of guidewire assembly 22 includes a tapered portion 42 to increase the flexibility and transition properties of the distal portion 26 of guidewire assembly 22.

Preferably, sealing system 60 is implemented as part of a handheld apparatus that also includes gas inflation/evacuation system 80. Alternatively, sealing system 60 may be a component completely separate from the gas inflation/evacuation system 80. Sealing system 60 includes a first aperture 62 into which the proximal end 36 ~~of the proximal portion 24~~ of guidewire assembly 22 is insertable so as to operably position at least a portion of <sup>extended</sup> sealable section 28 in relation to sealing system 60. Sealing system 60 further includes a second aperture 64 that is fluidly <sup>connectible</sup> ~~connectable~~ to gas inflation/evacuation system 80. <sup>The</sup> ~~In a preferred~~ means for selectively sealing the <sup>extended</sup> sealable section which in the preferred embodiment comprises ~~embodiment~~ sealing system 60 includes a crimping mechanism 66 and a sealing mechanism 68.

A passageway 70 is defined from first aperture 62 to second aperture 64 and <sup>extends</sup> ~~having a passage~~ through both crimping mechanism 66 and sealing mechanism 68. Preferably, at least a portion of the <sup>extended</sup> sealable section 28 is inserted into first aperture 62 a sufficient distance to engage crimping mechanism 66 and sealing mechanism 68.

5 In a preferred embodiment of the crimping mechanism 66 as shown in Figs. 12-14, the crimping mechanism 66 comprises a handle 72 that actuates a pivotable cam arrangement 74 that crimps and then severs the <sup>extended</sup> sealable section 28 between a pair of rollers 76, 78. Preferably, the sealing mechanism 68 <sup>has</sup> ~~is~~ a rotatable hemostatic valve positioned proximal to the crimping mechanism 66 along passageway 70. Preferably, crimping mechanism 66 and sealing mechanism 68 are arranged <sup>coaxially</sup> ~~coaxially~~ with each other along a straight portion of passageway 70. In this embodiment, when the proximal end 36 ~~of proximal portion 24~~ of guidewire assembly 22 is inserted into first aperture 62 until the proximal end 36 engages the hemostatic valve of sealing mechanism 68, the <sup>extended</sup> sealable section 28 is properly positioned relative to the crimping mechanism 66.

15 It will be seen that the relative distance between the engaging portions of sealing mechanism 68 and crimping mechanism 66 in this embodiment effectively defines the relative distances between a plurality of locations along <sup>extended sealable</sup> ~~sealing~~ section 28 at which an airtight seal can be created, as shown in Figs. 1-2. To permit multiple inflations and deflations of the occlusive balloon 32 of the guidewire assembly 22, the length of the extended sealable section 28   
20 ~~preferably~~ should be greater than at least twice the distance between crimping mechanism 66 and sealing mechanism 68.

The gas inflation/evacuation system 80 is connected via conduit 82 to the second aperture 64 of the sealing system 60. The gas inflation/evacuation system 80 preferably includes a valve <sup>which includes means for evacuating the guidewire assembly 22</sup> arrangement 84 that selectively couples one of an evacuation system ~~86~~ and an inflation system <sup>which includes means for introducing gas into the guidewire assembly 22</sup> ~~88~~ to the conduit 82. The evacuation system ~~86~~ <sup>includes an evacuation syringe 86 which</sup> is used to evacuate ~~air from~~ the guidewire assembly 22, passageway 70, and conduit 82. The inflation system ~~88~~ <sup>includes an inflation syringe 88 which</sup> contains a volume of a biocompatible gas sufficient to inflate the occlusive balloon 32 a plurality of times. Preferably, the biocompatible gas is carbon dioxide. Other biocompatible gasses that may be utilized with the present invention include ~~oxygen, nitrogen, and nitrous oxide~~. Although not preferred, low

viscosity biocompatible liquids or foams <sup>9/50</sup> may <sup>15</sup> also be used for inflation provided the surface tension of the fluid <sup>15</sup> was sufficient to permit the rapid inflation and deflation contemplated by the present invention. Optionally, a pressure gauge 90 can be associated with the inflation <sup>syringe</sup> system <sup>88</sup>.

5 In a preferred embodiment shown in Figs. 3a, 3b, 4a and 4b, guidewire assembly 22 is constructed as described in further detail in the previously identified <sup>10/012,891</sup> co-pending application, entitled "Guidewire <sup>Assembly</sup> Having Occlusive Device And Repeatably Crimpable Proximal End". The main body portion 30 is formed of a primary stainless steel hypotube having an outer diameter of 0.013 inches and an inner diameter of 0.007 inches. To accomplish passive deflation in the  
10 desired time of less than one minute when the <sup>extended</sup> sealable section 28 is cut, it is preferable that the main body portion 30 have an inner diameter of at least 0.002 inches. The <sup>extended</sup> sealable section 28 of guidewire <sup>assembly</sup> 22 is comprised of a crimp tube also formed of stainless steel and having an outer diameter of 0.009 inches to <sup>0.015 inch</sup> 0.115 inches and an inner diameter of at least 0.002 inches and preferably about 0.005 inches. The <sup>extended</sup> sealable section 28 is preferably secured to the proximal  
15 portion 24 by a laser weld 44 of sufficient strength. Alternatively, the <sup>extended</sup> sealable section 28 may be formed by <sup>centerless</sup> grinding or reducing the outer diameter of a portion of the proximal portion 24 of the main body <sup>portion</sup> 30 of guidewire assembly 22. Still other embodiments may <sup>also</sup> enable the <sup>extended</sup> sealable section to be a modified, treated or otherwise <sup>fabricated</sup> indicated portion of the proximal portion 24 of the main body <sup>portion</sup> 30 of guidewire assembly 22 that is suitable for the particular sealing  
20 technique to be used. As shown in Fig. 4a, in one embodiment the distal end of the <sup>extended</sup> sealable section 28 is preferably <sup>centerless</sup> ground and press fit within a chamfered proximal end of the main body portion 30. Alternatively, as shown in Fig. 4b, <sup>a</sup> chamfered crimp arrangement <sup>could be used. Still further,</sup> or a separate joining/crimping tube or <sup>other</sup> similar <sup>polytetrafluoroethylene</sup> tubular joining arrangements could be used. Preferably, a protective polymer coating 56 of <sup>polytetrafluoroethylene</sup> (PTFE) or a hydrophilic coating is applied by  
25 any of a number of known techniques such that the coating 56 surrounds the main body portion 30. The protective polymer coating 56 is preferably about 0.0004 +/- 0.0003 inches <sup>0.0132-0.0144</sup> thick such that the effective outer diameter of the main body portion 30 of guidewire assembly 22 is <sup>0.014</sup> inches.

In this embodiment, the <sup>extended</sup>sealable section 28 can be made of any material that when deformed and severed retains that deformation so as to form an airtight seal. When crimped and severed, it is preferable that the <sup>extended</sup>sealable section 28 not present a sharp, rigid point that is capable of piercing a gloved hand. It has been found that as long as the preferred embodiment is not gripped within less than one inch of the <sup>proximal</sup>~~proximate~~ end <sup>extended</sup>36 of the sealable section 28, the severed <sup>proximal</sup>~~proximate~~ end <sup>the extended</sup>36 of sealable section 28 does not penetrate a standard surgical glove. In addition, the <sup>extended</sup>sealable section 28 must have sufficient strength in terms of high tensile and kink resistance to permit catheter devices to repeatedly pass over the <sup>extended</sup>sealable section 28.

In this embodiment, the main body portion 30 is preferably secured to the distal portion 26 using a Ni-Ti <sup>main</sup>or stainless steel sleeve 46 <sup>main</sup>laser welded to the body portion 30 at laser weld 48 and crimped to the distal portion 26 at crimp 50. The distal portion 26 is preferably formed of a Ni-Ti alloy having an inner diameter of <sup>0.0045 inch</sup>~~0.045 inches~~ and an outer diameter that ranges from 0.014 inches ~~57~~ to 0.0075 inches ~~57~~ to form tapered portion 42, preferably formed by a centerless grinding process. Preferably, the distal portion includes a pair of coil sections, proximal tip coil 52 and distal tip coil 54, that are longitudinally spaced apart and adjacent to the holes 35 and that assist in providing a better surface for bonding the <sup>occlusive</sup>balloon 32 to the distal portion 26. This arrangement also tends to increase the visibility of the location of <sup>the occlusive</sup>balloon 32 under fluoroscopy, as the <sup>occlusive</sup>balloon 32 filled with a biocompatible gas will be radiotranslucent when compared to the two coils 52 and 54. Alternatively, a platinum markerband could be located around the distal portion 26 just proximal to the occlusive balloon 32 to serve as a radiopaque/MRI marker. The flexible tip 38 is <sup>a</sup>coiled tip attached to distal portion 26 distal to <sup>occlusive</sup>balloon <sup>flexible</sup>32, preferably by a crimp ~~54~~. Alternatively, a sleeve could be welded to the tip 38, and the tapered portion 42 could then be inserted into this sleeve and crimped.

Alternatively, any number of other alloys or polymer materials and attachment techniques could be used in the construction of the guidewire assembly 22, provided the materials offered ~~the~~ <sup>the</sup>flexibility and torque characteristics required for a guidewire and the attachment techniques ~~were~~ <sup>are</sup>sufficiently strong enough and capable of making an airtight seal. These materials include, but are not limited to, ~~a tubular guidewire of all~~ <sup>the</sup>Ni-Ti, 17-7 stainless steel, 304 stainless steel, cobalt superalloys, or other polymer, braided or alloy materials. The attachment techniques for

constructing guidewire assembly 22 include, but are not limited to, welding, mechanical fits, adhesives, sleeve arrangements or any combination thereof.

The <sup>occlusive</sup>balloon 32 may be made of any number of <sup>occlusive</sup>expandable polymer or rubber materials. Preferably, the <sup>occlusive</sup>balloon is preinflated to prestretch <sup>it so that</sup>the balloon so balloon expansion is more linear with pressure. Preferably, the pressure supplied by gas system 80 is designed to stay well within <sup>the</sup>elastic limits <sup>the occlusive</sup>of balloon 32. A two-layer <sup>occlusive</sup>balloon arrangement, adding gas and/or liquid between balloon layers, may be used in an alternate embodiment to increase visibility of the distal end <sup>40</sup>of the <sup>distal portion 26 of the</sup>guidewire assembly 22 under fluoroscopy.

In practice, medical personnel gain entry to the vessel lumen prior to use of the guidewire occlusion system 20. The <sup>extended sealable section 28 of the</sup>proximal portion 24 of guidewire assembly 22 is inserted into first aperture 62 and connected via sealing mechanism 68. The distal portion 26 of guidewire assembly 22 is inserted into the vessel lumen, and occlusive balloon 32 is inserted to a point distal to the vessel occlusion. Valve arrangement 84 is set for evacuation. <sup>Evacuation</sup>First syringe plunger 92 of evacuation <sup>syringe</sup>system 86 is slidably withdrawn removing any air from guidewire assembly 22. Valve arrangement 84 is then set for inflation. <sup>Inflation</sup>Second <sup>syringe</sup>syringe plunger 94 of inflation <sup>system</sup>88 is slidably advanced inserting a volume of an inert gas into guidewire assembly 22. The inert gas inflates occlusive balloon 32 as shown in Fig. 2. During inflation, the medical personnel monitor pressure gauge 90 to <sup>e</sup>insure that the inflation pressure does not exceed the burst rating of the occlusive balloon 32 and to gauge the relative size of the occlusive balloon 32 as it is inflated. Following inflation of occlusive balloon 32, crimping mechanism 66 is employed to crimp the <sup>extended</sup>sealable section 28 of guidewire assembly 22, thereby sealing the guidewire assembly 22 to maintain the occlusive balloon 32 in an inflated state. Sealing mechanism 68 is released and the <sup>extended sealable section 28</sup>proximate portion 24 is removed from first aperture 62 <sup>as shown in Figure 3</sup>such that the proximal portion 24 of the guidewire assembly 22 is free of mechanical or other obstructions and <sup>can</sup>functions as a conventional guidewire. When the medical personnel decide to deflate the occlusive balloon 32, the <sup>extended</sup>sealable section 28 is cut using a medical scissors or the like distal to the existing crimp in the <sup>extended</sup>sealable section 28. When the medical personnel deem reinflation of the occlusive balloon 32 to be necessary, <sup>the extended sealable section 28 of the</sup>proximal portion 24 is reinserted into first aperture 62. Sealing mechanism 68 is then <sup>reactivated</sup>activated and the

evacuation/inflation process can be repeated. It will be understood that a crimping handle 72 may also be provided with a separate severing arrangement to cut the <sup>extended</sup> sealable section 28. Alternatively, <sup>extended</sup> sealable section 28 may be scored or otherwise weakened in selected locations to assist in crimping or severing, including severing by repeated bending back and forth at one of the scored locations. In another embodiment, the <sup>extended</sup> sealable section 28 could be broken off rather than sheared by using a brittle metal for the <sup>extended</sup> sealable section that <sup>aids</sup> in the severing of sealable section 28.

*system 80a and also an alternative sealing system 60a*

Fig. 5 shows an alternative unitized gas inflation/evacuation <sup>inflation syringe 114 with plunger individual 112 with evacuation syringe plunger</sup> assembly 80. Assembly body 96 contains individual inflation syringe 98 and evacuation syringe 100. Assembly body 96 contains pressure gauge 90. Attached to assembly body 96 is <sup>support</sup> structure 102 which <sup>supports a sealing system 60a that</sup> includes crimping mechanism <sup>66a</sup> and sealing mechanism <sup>68a</sup>. Valve arrangement 84 is mounted on the surface of assembly body 96. Assembly body 96 contains two finger grip bores 104. Attached to assembly body 96 is finger grip 106. In the preferred embodiment, the assembly body 96 is constructed of a suitable inert plastic polymer, although any polymer material used in construction of medical devices could be used. In another embodiment, the assembly body 96 can be constructed of suitable metal alloys or even of tempered glass or any combination thereof.

*80b in use with sealing system 60a*

Fig. 6 shows an alternative gas inflation/evacuation system <sup>arrangement</sup> 80. Valve switch 108 has three <sup>interconnect 110a, 110b and 110c</sup> valve fittings <sup>110</sup>. Attached to <sup>one</sup> interconnect fitting <sup>110</sup> is evacuation chamber 112. <sup>Evacuation syringe includes plunger</sup> Mounted within evacuation chamber 112 is evacuation syringe 100. Attached to <sup>another</sup> interconnect fitting <sup>110</sup> is pressure gauge 90. Pressure gauge 90 is fluidly interconnected to inflation chamber 114. <sup>Inflation syringe includes plunger</sup> Mounted within inflation chamber 114 is inflation syringe 98. Attached to the <sup>last</sup> interconnect fitting <sup>110</sup> is structure 116. Structure 116 is comprised of crimping mechanism <sup>66a</sup> and sealing mechanism <sup>68a</sup>. Preferably, one-way check valves 111 and 113 <sup>are respectively</sup> connected between interconnect fitting <sup>110</sup> and <sup>each of</sup> evacuation chamber 112 and inflation chamber 114 as a safety measure to insure only one-way flow of the gas within the system <sup>80</sup>. Check valve 113 <sup>insures that only the carbon dioxide gas is delivered out of the device and prevent any reinfusion of air that has been evacuated from the system.</sup>

*80c with sealing system 60*

Figs. 7 and 8 show an alternative gas inflation/evacuation system <sup>80</sup>. Assembly body 118 contains inflation <sup>chamber 114</sup> and evacuation <sup>chamber 112</sup>. Inflation <sup>chamber 114</sup>

includes plunger syringe includes plunger  
 contains inflation syringe 98. Evacuation chamber 112 contains evacuation syringe 100. Valve  
 switch 108 is mounted on the exterior of assembly body 118. Pressure gauge 90 is contained  
 within assembly body 118. Assembly body 118 contains finger grips 106. Conduit 122 is  
 attached to assembly body 118. At the distal end of conduit 122 is ~~structure 124~~ <sup>sealing system 60 which</sup>  
 is comprised of crimping mechanism 66 and sealing mechanism 68.

Fig. 9 shows an embodiment of the sealing system ~~60~~ <sup>Specifically, Fig. 9 shows sealing</sup> ~~Sealing system 60 is preferably~~  
 comprised of sealing mechanism 68 and crimping mechanism 66. Crimping mechanism 66 is  
 comprised of crimp body 126, handle 72, handle return 128, and ~~crimp~~ <sup>first 62</sup> aperture 130. Sealing  
 mechanism 68 is comprised of sealing body 132 and ~~sealing~~ <sup>second 64</sup> aperture 134. Sealing system 60 has  
 a ~~passageway 70 (see Figs. 1 and 2)~~ <sup>first 62</sup> and ~~sealing~~ <sup>second 64</sup> aperture 134. Sealing system 60 has  
 10 ~~sealing bore 136~~ fluidly interconnecting ~~crimp~~ <sup>first 62</sup> aperture 130 and ~~sealing~~ <sup>second 64</sup> aperture 134.

Fig. 10 shows an alternative gas inflation/evacuation assembly ~~60~~ <sup>80d coupled to sealing system 60</sup>. Valve switch 108 has  
 a port 138 that is attached via ~~check valve 111~~ <sup>coupling 141 connected to conduit 82 and a one-way</sup> and hose 140 to evacuation syringe ~~100~~ <sup>112</sup>.  
 Attached to ~~one~~ <sup>an interconnect fitting 139</sup> of the valve switch 108 is inflation manifold 142. Inflation manifold 142 is  
 connected ~~connector 146~~ <sup>to</sup> and pressure gauge 90. Inflation manifold 142 has three check valves  
 144a, 144b and 144c. ~~Each check valve 144 is~~ <sup>check valves 144a, 144b, and 144c are</sup> connected to a respective inflation syringes ~~98a,~~ <sup>114a, 114b and 114c which have respective</sup>  
 98b, and 98c. In this embodiment, evacuation syringe ~~100~~ <sup>112</sup> is mounted behind pressure gauge 90. <sup>inflation syringe plungers</sup>  
 As with the other embodiments, the distal end of conduit 82 is connected to sealing system 60.  
 Sealing system 60 is comprised of sealing mechanism 68 and crimping mechanism 66.

Fig 11 shows an alternative gas inflation/evacuation system ~~60~~ <sup>80e</sup> that is similar to the  
 20 ~~embodiment~~ <sup>gas inflation/evacuation system 80d</sup> shown in Figure 10 except that the components are arranged in a common housing  
 150. ~~Housing 150~~ <sup>Common housing 150</sup> has internal channels that fluidly interconnect ~~via coupling 141, conduit 82~~ <sup>sealed</sup>  
 to valve switch 108, and connect valve switch 108 to evacuation syringe ~~100~~ <sup>112</sup> and inflation  
 syringes ~~98a, 98b, and 98c~~ <sup>114a, 114b and 114c</sup> and pressure gauge 90. ~~Housing 150~~ <sup>Common housing 150</sup> contains structure 152 that  
 defines ~~the~~ <sup>the</sup> chambers for three inflation syringes ~~98a, 98b, and 98c~~ <sup>114a, 114b and 114c</sup>. ~~Housing 150~~ <sup>Common housing 150</sup> also contains  
 25 ~~structure defining external finger grips 106 and internal finger grip structures 154 between~~ <sup>Common housing 150</sup>  
 adjacent ~~inflation syringes 98~~ <sup>portions of structure 152</sup>. ~~Housing 150~~ <sup>Common housing 150</sup> also contains structure for integrating evacuation  
 syringe ~~100~~ <sup>112</sup> and pressure gauge 90 as part of ~~unitary~~ <sup>the common</sup> housing 150. ~~An external knob 156 connects~~ <sup>to the valve arrangement 108.</sup>

Figs. 18 and 19 show ~~alternative~~ <sup>an</sup> embodiments to that shown in Fig. 11. Rather than  
 utilizing the ~~housing 150~~ <sup>common</sup> for the formation of internal sealed channels, an assembled gas



80f the gas inflation/evacuation system 80d  
inflation/evacuation system 80, substantially similar to that shown in Fig. 10, is securely placed  
a two-part within housing 150 such that housing 150 provides a protective and functional casing around the  
system 80. As demonstrated in the exploded view of Fig. 18, the previously described  
gas inflation/evacuation components of the system 80 are assembled prior to fitting of the housing. In addition to the  
5 components described above, this exploded view shows: namely, the connector 143 and coupling 145  
connector 143 is intermediately connected to pressure gauge 90 at one end and connector 146 at  
the other end. Further, coupling 145 interconnects valve switch 108 to tee connector 143. Upon  
completion of the component assembly, the assembled system is securely placed within a top  
cover housing 151, as shown in Fig 19. Once secured, a compatible bottom cover housing 153 is  
10 joined with top housing 151 to form the final housing 150, also shown in Fig. 19. This joining of  
top housing 151 and bottom housing 153 can be achieved using a myriad of techniques, such as  
adhesive bonding, heat bonding, chemical bonding, pressure fittings, snap connectors, clip  
connectors, fasteners such as screws and bolts, and the like.

The embodiments shown in Figs. 10, 11, 18, and 19 allow for effective pressurization of  
15 a balloon 32 at less than 2 atmospheres while reducing the total volume of gas that might be  
introduced into a patient in the event of a leak in the system 20. Depending upon the desired  
inflation pressure and the total number of inflation cycles, the total amount of pressurized gas in  
a single the inflation syringe 98 can be significant. If a leak were to occur, the entire contents of inflation  
syringe 98 would be susceptible to that leak. By using a separate syringe 98a, 98b, 98c for each  
20 inflation in the embodiments shown in Figs. 10 and 11, these alternate embodiments provide a  
simple way of decreasing the total amount of pressurized gas that might be introduced into a  
patient in the event of a leakage in the system 20.

A similar result could be achieved by manually attaching separate inflation syringes 98a,  
98b, 98c and manually attaching the evacuation syringe 100 directly to the sealing system 60 by  
25 way of a luer lock or the like. While this embodiment would not be as quick or convenient as the  
preferred embodiment, this alternative would eliminate the volume of gas required for the  
conduit 82 and within housing 150, as well as the need for a valve switch 108.

In alternate embodiments, the sealing system 60 could use techniques other than crimping  
to accomplish multiple airtight seals along the course of the extended sealable section 28. One

The O-rings 166 and 168 serve as wiping structure to remove excess sealant material from the outside of the extended sealable section 28.

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alternate embodiment, as <sup>portrayed</sup> ~~contained~~ <sup>FIG.</sup> in Figure 15, would involve the insertion of some form of sealant material 158 into the proximal end of the <sup>extended</sup> sealable section 28, such as wax, plastic, polymer or metal inserts or plugs. Conduit 82 is attached to <sup>a plugging</sup> sealing mechanism 162 through the conduit aperture 160. In this embodiment, sealant material 158 is <sup>confined</sup> ~~restrained~~ by sealant <sup>containment</sup> ~~residing~~ <sup>mechanism 162</sup> layer 164 <sup>plugging</sup> ~~residing~~ within sealing body 166. Preferably for this embodiment, sealant material 158 is a wax or gel that is flowable at higher temperatures and might be melted during sterilization of the sealing system 60. Sealant <sup>containment</sup> ~~layer~~ 164 is a foil layer or thin layer of non-meltable material capable of <sup>confining</sup> ~~restraining~~ a flowable material during any sterilization process or exposure to higher temperature. The proximal end of <sup>extended</sup> sealable section 28 is inserted through first aperture 62 until it is past operational <sup>O</sup> ~~ring~~ 166 or some other form of sealable/deformable material such as a silicone puncture seal or similar membrane seal. When it is desired to seal the <sup>extended</sup> sealable section 28, the <sup>extended</sup> sealable section 28 is further inserted past a <sup>second</sup> ~~second~~ <sup>optional</sup> sealant <sup>O</sup> ~~ring~~ 168, <sup>then</sup> through sealant <sup>containment</sup> ~~layer~~ 164, and <sup>finally</sup> into sealant material 158. Sealant material 158 is deposited in the proximal end of <sup>extended</sup> sealable section 28, <sup>thus</sup> preventing the guidewire assembly 22 from being evacuated. <sup>Extended</sup> Sealable section 28 can then be slidably <sup>sealant O-ring 168, through the O</sup> ~~withdrawn~~ through the <sup>and through</sup> operational <sup>O</sup> ~~ring~~ 166, and <sup>thereby</sup> first aperture 62, effectively disengaging the guidewire assembly 22 from the <sup>plugging</sup> ~~sealing~~ mechanism 162. Other alternate embodiments involve

~~The constriction of a location along the extended sealable section 28 by heating where the~~ <sup>extended</sup> sealable section 28 <sup>when it is</sup> ~~is~~ formed of metal or polymer material so as to create a constriction, or ~~by~~ <sup>applying</sup> application of electrical or magnetic energy to arc or weld material within the <sup>extended</sup> sealable section 28 to create a constriction. In one embodiment, the equivalent of a spot welder could be used in place of the crimping mechanism 66 to accomplish the same purpose of sealing, and then severing the <sup>extended</sup> sealable section 28. Alternative embodiments could use other sealing techniques to seal the guidewire assembly 22. These methods could include, but are not limited to, ones utilizing a heat source to melt the <sup>extended</sup> sealable section, ones using a heat source to apply a glue or gel, methods ~~involving~~ <sup>involving</sup> insertion of a plug material, methods using magnetics to manipulate a sealing material, or methods utilizing small occlusive devices.

Depending on the sealing method specified in <sup>an</sup> ~~the~~ embodiment, different deflation techniques can be utilized. For the preferred embodiment, the <sup>extended</sup> sealable section 28 is of sufficient

length to allow deflation through the shearing, breaking or opening of the <sup>extended</sup> sealable section 28 distal to the sealant material 158 located in the proximal end of the <sup>extended</sup> sealable section 28. By having sufficient length of the <sup>extended</sup> sealable section 28, the guidewire assembly 22 can be coupled to the gas inflation/evacuation system 80 <sup>(or 80a-80f)</sup> multiple times, allowing the occlusive balloon 32 to be  
5 inflated and deflated multiple times. Other embodiments will use methods of deflation including melting the sealant material 158, removing a plug of sealant material 158, and various other methods not requiring the <sup>extended</sup> sealable section 28 to be sheared.

In one embodiment, the guidewire occlusion system 20 is preferably pre-assembled and packaged in an environment consisting of an appropriate biocompatible gas. Fig. 16 shows an  
10 ~~embodiment of the~~ <sup>equipment with which</sup> guidewire occlusion system 20 <sup>is</sup> being assembled and packaged. The guidewire occlusion system 20 is assembled and packaged in <sup>a</sup> sealed chamber 170. Sealed chamber 170 is ~~generally~~ <sup>a</sup> equipped with <sup>a</sup> venting ducts 171, sealed handling ports 173, and an atmosphere control system 175. The venting ducts 171 and atmosphere control system 175 provide the overall system for maintaining a biocompatible gas atmosphere within the sealed  
15 chamber 170. Sensory readings within the <sup>sealed</sup> chamber 170 provide the atmosphere control system 175 with the data needed to adjust the biocompatible gas levels within the <sup>sealed</sup> chamber 170. Stored biocompatible gas is introduced into the <sup>sealed</sup> chamber 170 through the venting ducts 171. Assembling and packaging of the guidewire occlusion system 20 and/or any of the pre-assembled components is achieved with the use of the sealed handling ports <sup>173</sup> 173. The ports <sup>173</sup> 173  
20 are sterilized and sealed so that an assembler or packager positioned outside the <sup>sealed</sup> chamber 170 can access the contents of the chamber without introducing contamination through actual human contact or through the introduction of undesirable gases and airborne contaminants. These ports <sup>173</sup> 173  
<sup>as shown,</sup> could be constructed of flexible glove-like attachments, or they could be robotic devices operable within the <sup>sealed</sup> chamber 170 through controls external to the <sup>sealed</sup> chamber 170. The <sup>equipment</sup> chamber  
25 170 could be <sup>sealed</sup> the connection of two or more chambers <sup>as seen in Fig. 17</sup> as seen in Fig. 17.

After <sup>a</sup> the guidewire ~~occlusion system 20~~ and its corresponding components are placed in the chamber 170, the guidewire <sup>a</sup> assembly 22, <sup>(or 60a)</sup> sealing system 60, and gas inflation/evacuation <sup>a</sup> system 80 <sup>(or 80a-80f)</sup> are placed in a sealed chamber 170, <sup>(Fig. 17)</sup> and assembled to form the guidewire occlusion system 20 and placed into biocompatible packaging 174. Biocompatible packaging 174 is hermetically sealed so that the

internal volume of both biocompatible packaging 174 and guidewire occlusion system 20 is <sup>composed</sup> ~~comprised~~ solely of biocompatible gas ~~[174]~~. A preferred embodiment of the <sup>biocompatible</sup> packaging 174 is shown in Fig. 17. The <sup>biocompatible</sup> packaging 174 is preferably <sup>in the form</sup> ~~comprised~~ of a <sup>foil</sup> foil pouch. This pouch is made from a medical packaging film with the following laminates: <sup>an</sup> 8.75 micron foil layer, an adhesive layer, a white polyethylene layer, and a 12 micron PET layer. The <sup>foil</sup> pouch ~~[174]~~ has a preferred total thickness of approximately 3.6 millimeters, and a minimum bond strength of <sup>one</sup> ~~[1]~~ pound. In addition, the preferred barrier properties of the film will be an oxygen transmission < .01cc/100sq. in/24 hr. (73 degrees F, 0% RH) ASTM 3985, and moisture vapor transmission < .01gm H2O/100sq. in/24hr. (100 degrees F, 90%RH) ASTM F1249. It will be understood by those skilled in the art that this biocompatible <sup>foil</sup> pouch ~~[174]~~ can be contained and/or attached within an outer packaging or container, such as a cardboard box, a plastic container, or the like. Such an outer packaging will facilitate shipping, labeling, storage, and handling of the biocompatible packaging 174 and its contents.

In practice, medical personnel gain access to the ~~[blood]~~ vessel lumen through which the guidewire assembly 22 will travel. The guidewire occlusion system 20 is removed from biocompatible packaging 174. Flexible tip 38 <sup>in the vessel lumen</sup> is inserted <sup>(or 108)</sup> and is manipulated to a point beyond the vessel occlusion. Valve arrangement 84 <sup>(or 100)</sup> is adjusted to the evacuation position and ~~[first]~~ <sup>evacuation</sup> syringe plunger 92 is slidably withdrawn to remove any gas present in the guidewire assembly 22. Valve arrangement 84 <sup>(or 108)</sup> is adjusted to the inflation position and ~~[second]~~ <sup>inflation (or 98, 98a, 98b, 98c)</sup> syringe plunger 94 is slidably inserted causing occlusive balloon 32 to inflate.

Following inflation of occlusive balloon 32, handle 72 <sup>of (or the handle of 66e)</sup> ~~[or]~~ the crimping mechanism 66 is depressed causing roller 76 and roller 78 to crimp and preferably sever the <sup>extended</sup> sealable section 28 of guidewire assembly 22. ~~[In this embodiment]~~ <sup>extended</sup> severing of the sealable section 28 serves as an immediate verification of the creation of an effective seal. Sealing mechanism 68 <sup>(or 68a)</sup> can be released and guidewire assembly 22 can be completely removed from the sealing system 60 <sup>(or 60a)</sup> allowing the occlusive balloon 32 to remain inflated while occlusive substance treatment occurs. Following treatment, the <sup>extended</sup> sealable section 28 can be sheared or broken off, resulting in the deflation of the occlusive balloon 32. If occlusive treatment is complete, guidewire assembly 22 can be removed from the vessel lumen. If additional treatment is required, <sup>extended</sup> sealable section 28

(or 60a)

(or 68a)

can be reattached to sealing system 60 through first aperture 62. Sealing mechanism 68 can be retightened and the evacuation/inflation process can be repeated.

In a preferred embodiment of the present invention, the guidewire assembly 22 is utilized as the guidewire for an atherectomy or thrombectomy procedure of the type described in U.S. Patent Nos. 5,370,609 or 5,496,267, the disclosures of each of which are hereby incorporated by reference. In each of these procedures, the guidewire assembly 22 is introduced into the patient, the occlusive balloon 32 is inflated, and then the atherectomy or thrombectomy catheter arrangement is slid over the proximal end 36 of the guidewire assembly 22 and advanced until it is proximate and proximal to the location of the occlusive balloon. The procedure is performed for a time period consistent with the desired maximum length for blockage of the particular vessel, at which time the sealable section 28 of the guidewire assembly 22 may be severed to deflate the occlusive balloon 32, thereby reestablishing blood flow within the vessel. Depending upon the nature of the procedure, the catheter arrangement may be removed from the vessel or left in place. Preferably, an evacuation of any debris or other plaque material dislodged by the therapy is accomplished before deflation of the occlusive balloon 32 and the occlusive balloon 32 is reinflated prior to reinitiation of the procedure.

The present invention may be embodied in other specific forms without departing from the essential attributes thereof; therefore, the illustrated embodiments should be considered in all respects as illustrative and not restrictive, reference being made to the appended claims rather than to the foregoing description to indicate the scope of the invention.